

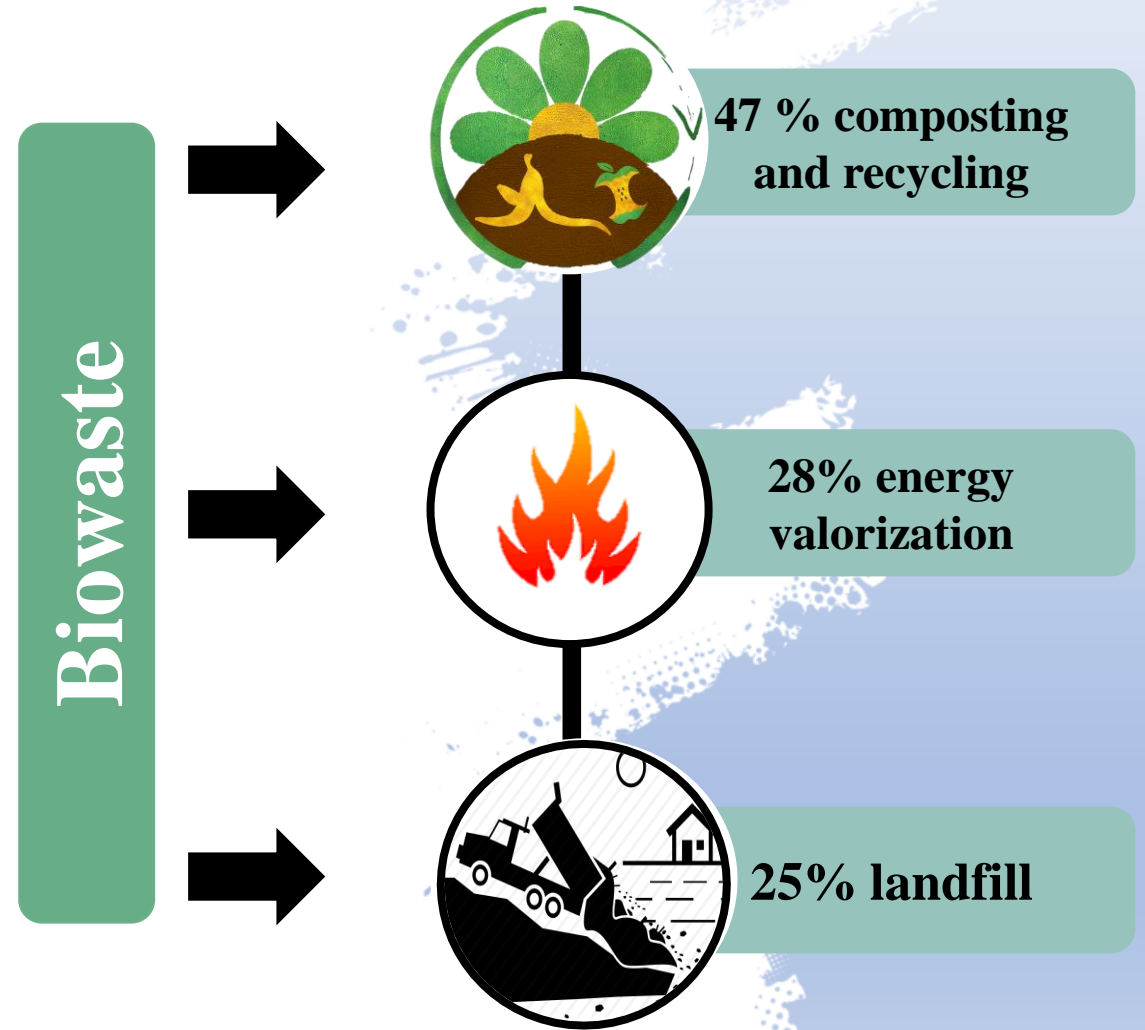
Energy recovery from lignocellulosic biomass by hydrothermal carbonization and anaerobic digestion: A circular economy concept

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$2.2 \cdot 10^8 \text{ t MSW year}^{-1}$

$\approx 10\%$ lignocellulosic biomass

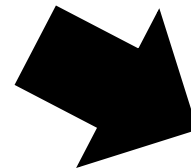
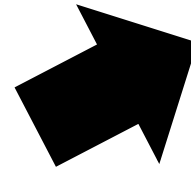


Urban Bioeconomy: from Biowaste to Biofuels and Bioproducts of Industrial Interest

**Urban pruning
waste**



**One the most
abundant energy
resource on the
planet**



Industrial level

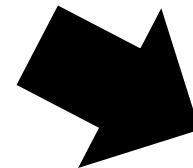
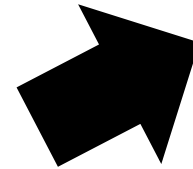


Home level

**Urban pruning
waste**



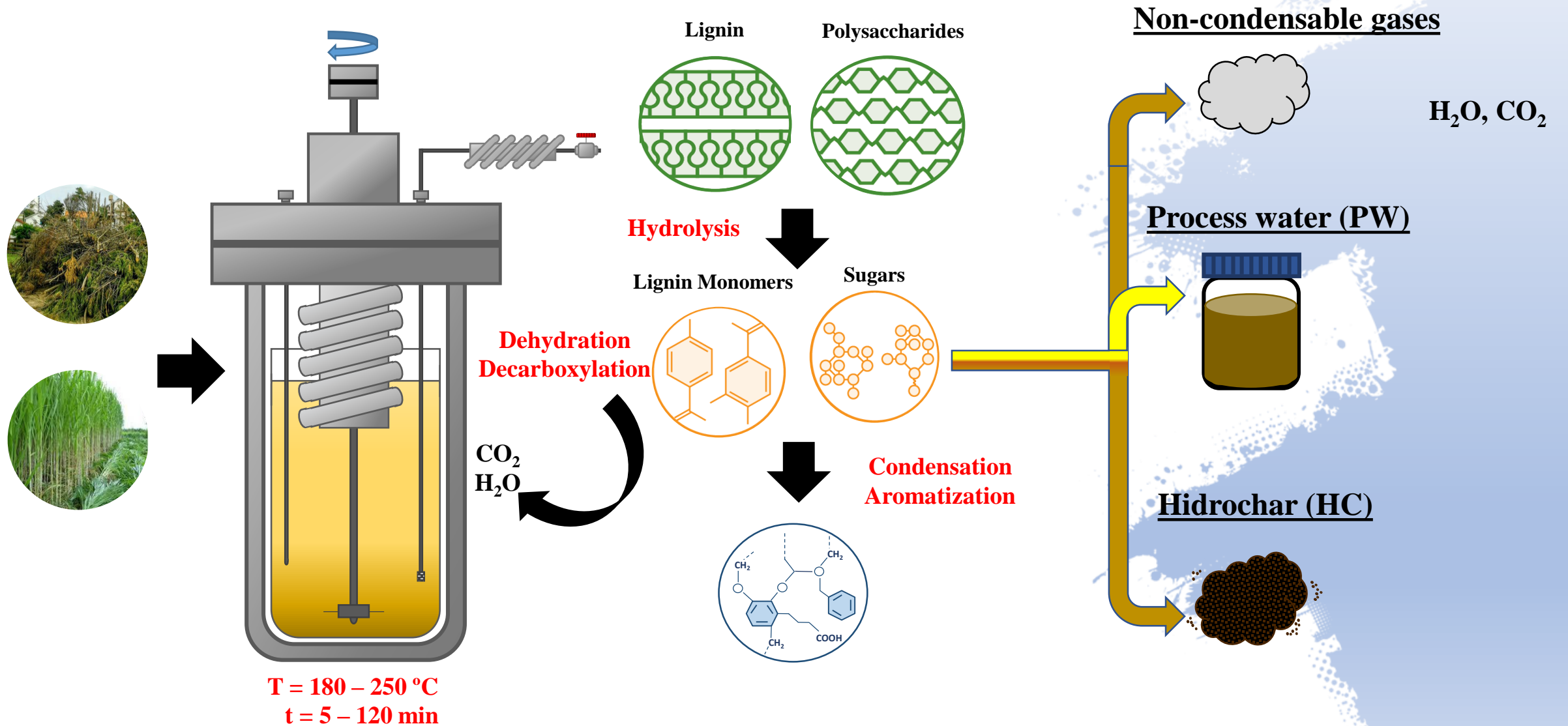
**One the most
abundant energy
resource on the
planet**



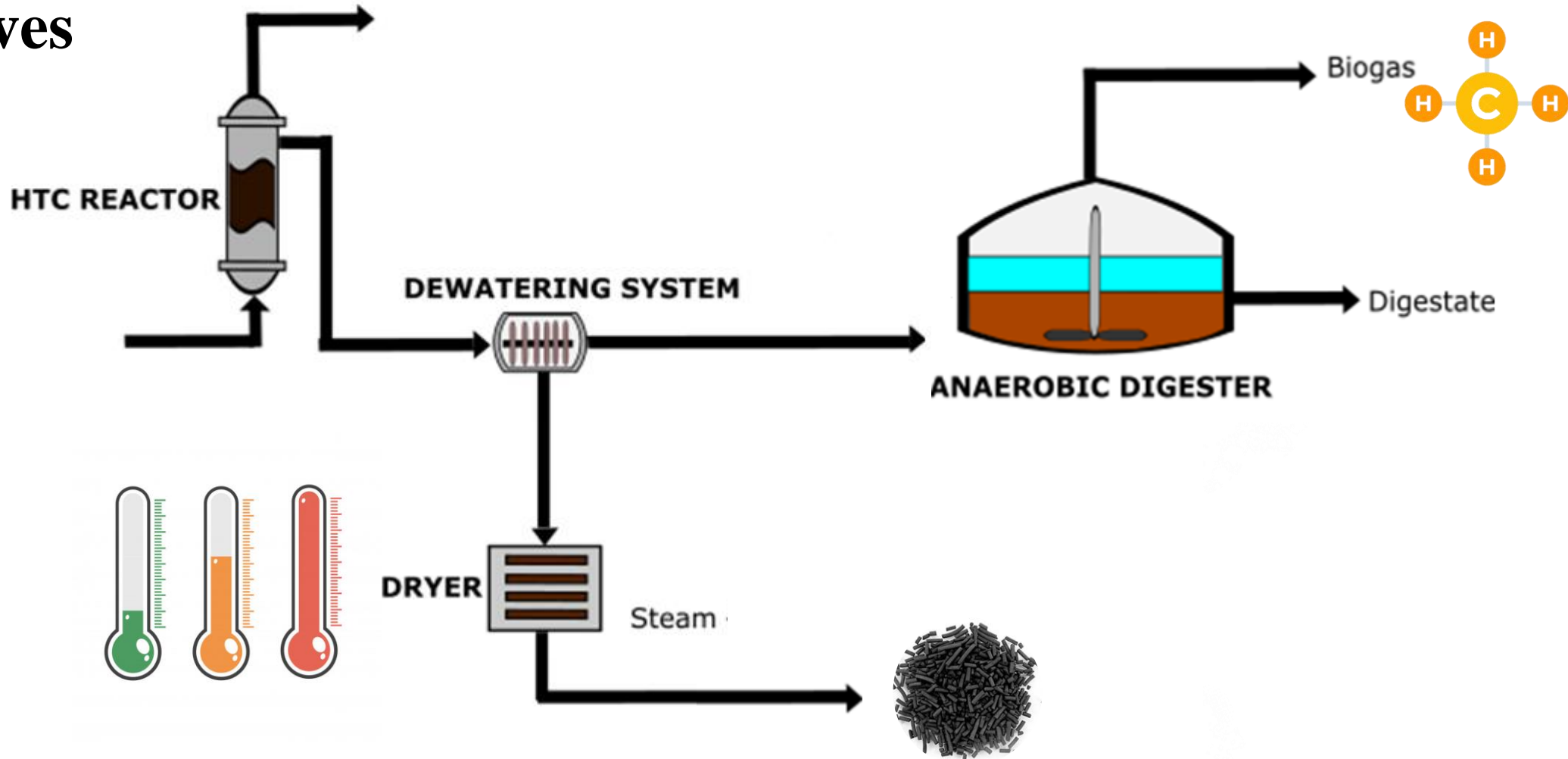
Industrial level



Home level

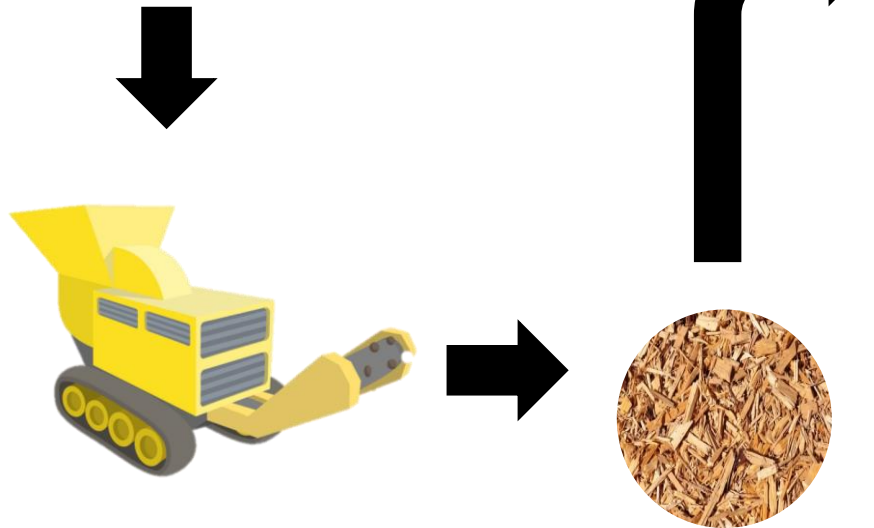


Objectives





Urban Pruning Waste

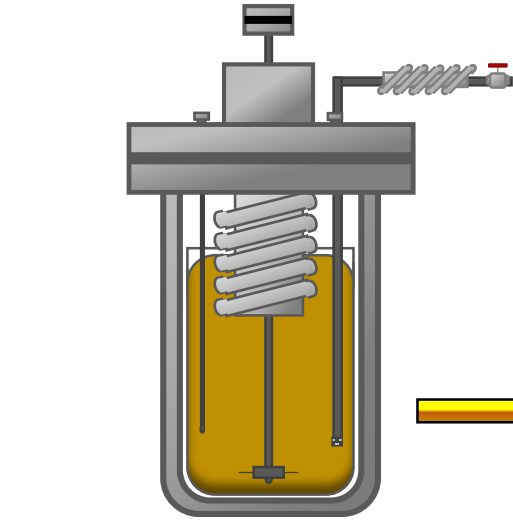


Characteristics	UPW
Moisture (%)	4.76 ± 0.2
C (%)	46.9 ± 1.1
H (%)	6.1 ± 0.4
N (%)	0.9 ± 0.1
S (%)	0.4 ± 0.2
O* (%)	40.6 ± 0.1
Volatile matter (d.b.%)	76.5 ± 0.1
Ash (d.b.%)	5.1 ± 0.1
Fixed carbon (d.b.%)	18.4 ± 0.1
HHV (MJ kg⁻¹)	19.7 ± 0.1
H/C	1.55
O/C	0.65
NPK	0.9/0.1/0.5
Ca (mg g ⁻¹)	10.13
Al (mg g ⁻¹)	0.12
Na (mg g ⁻¹)	0.03
Mg (mg g ⁻¹)	0.77
Fe (mg g ⁻¹)	0.10
K (mg g ⁻¹)	4.86
P (mg g ⁻¹)	0.93

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Urban Pruning Waste



$T = 180 - 210 - 230 \text{ } ^\circ\text{C}$
 $t = 60 \text{ min}$



UPW (20% weight) + H₂O (80% weight)

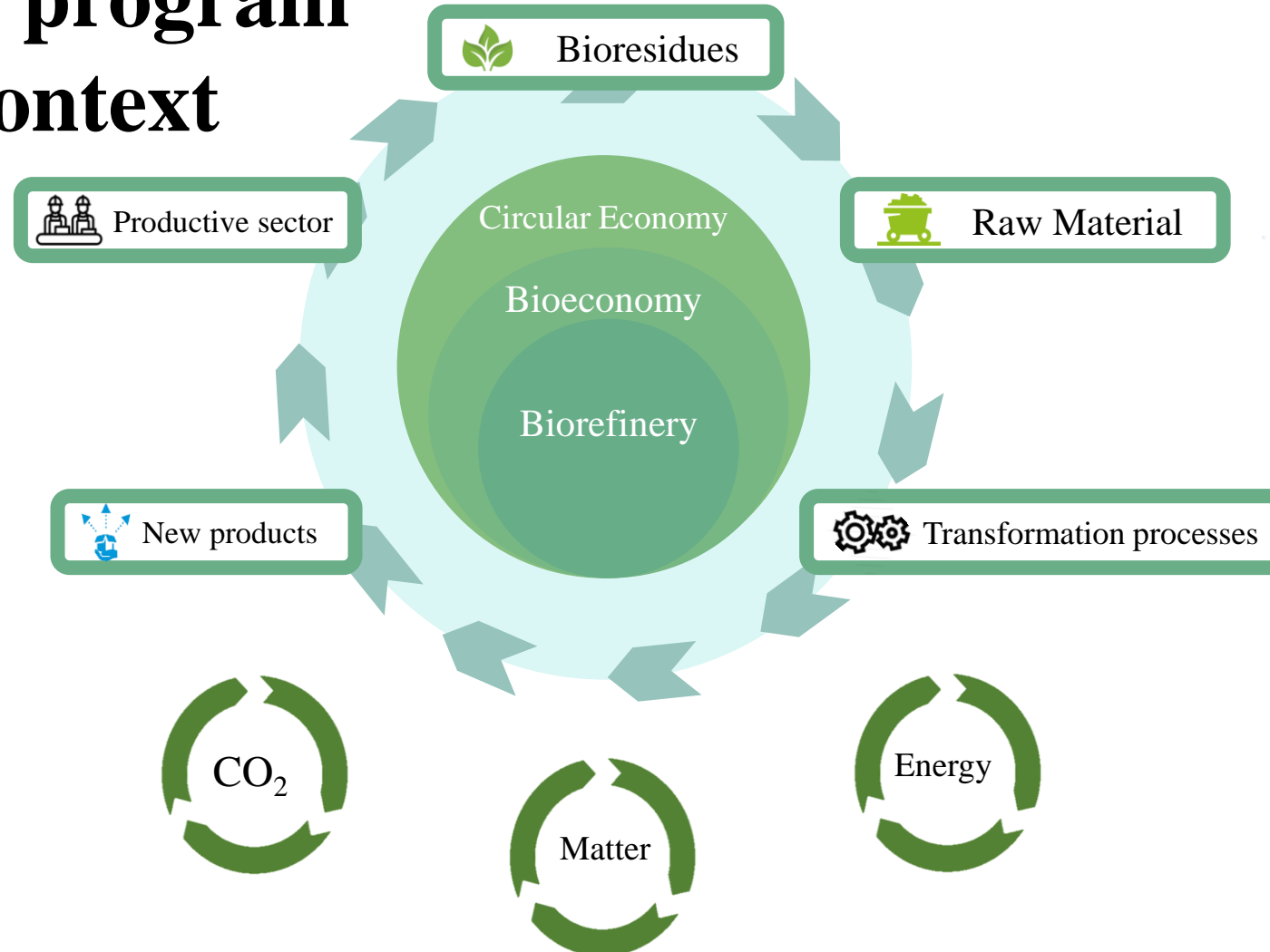
Process water (PW)



Hydrochar (HC)



BIO3 program context



Objective 3

Hydrothermal carbonization of biowaste

Objective 7

Anaerobic digestion of process water from hydrothermal carbonization

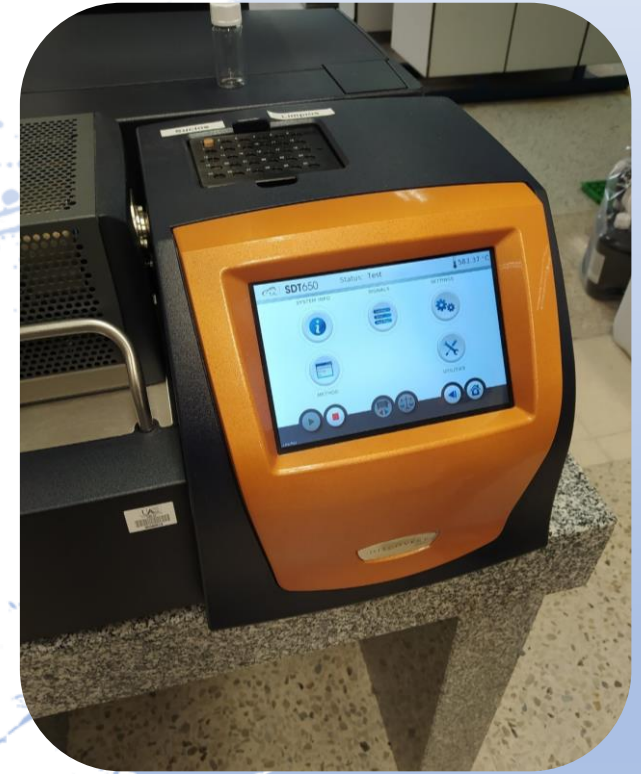
Materials and methods



HTC reactor



Anaerobic digestion



Thermogravimetric analysis (TGA)

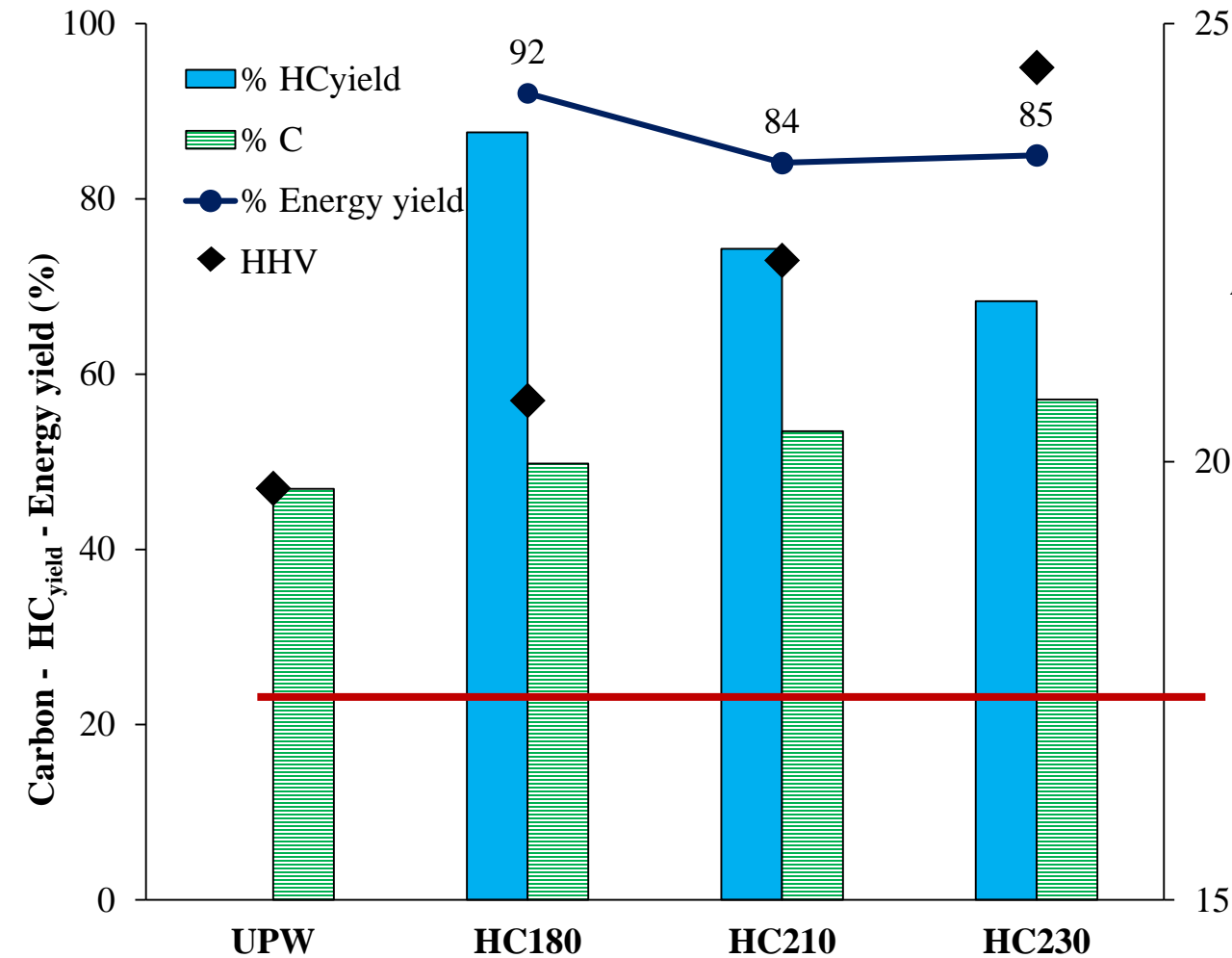


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Results



Energy and elemental analysis



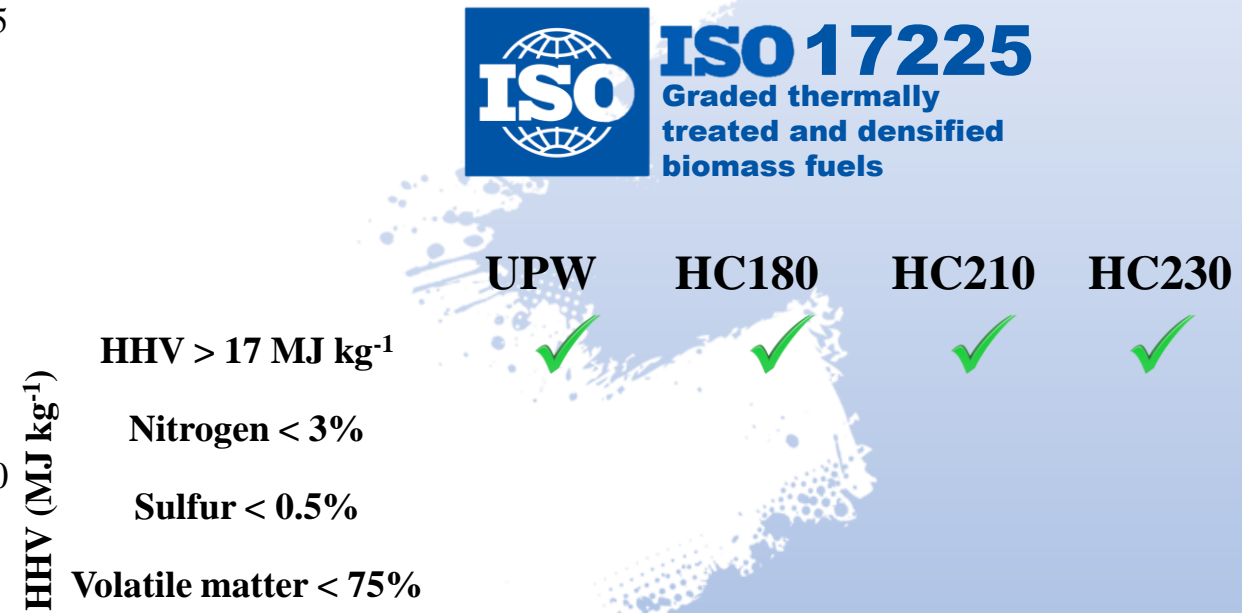
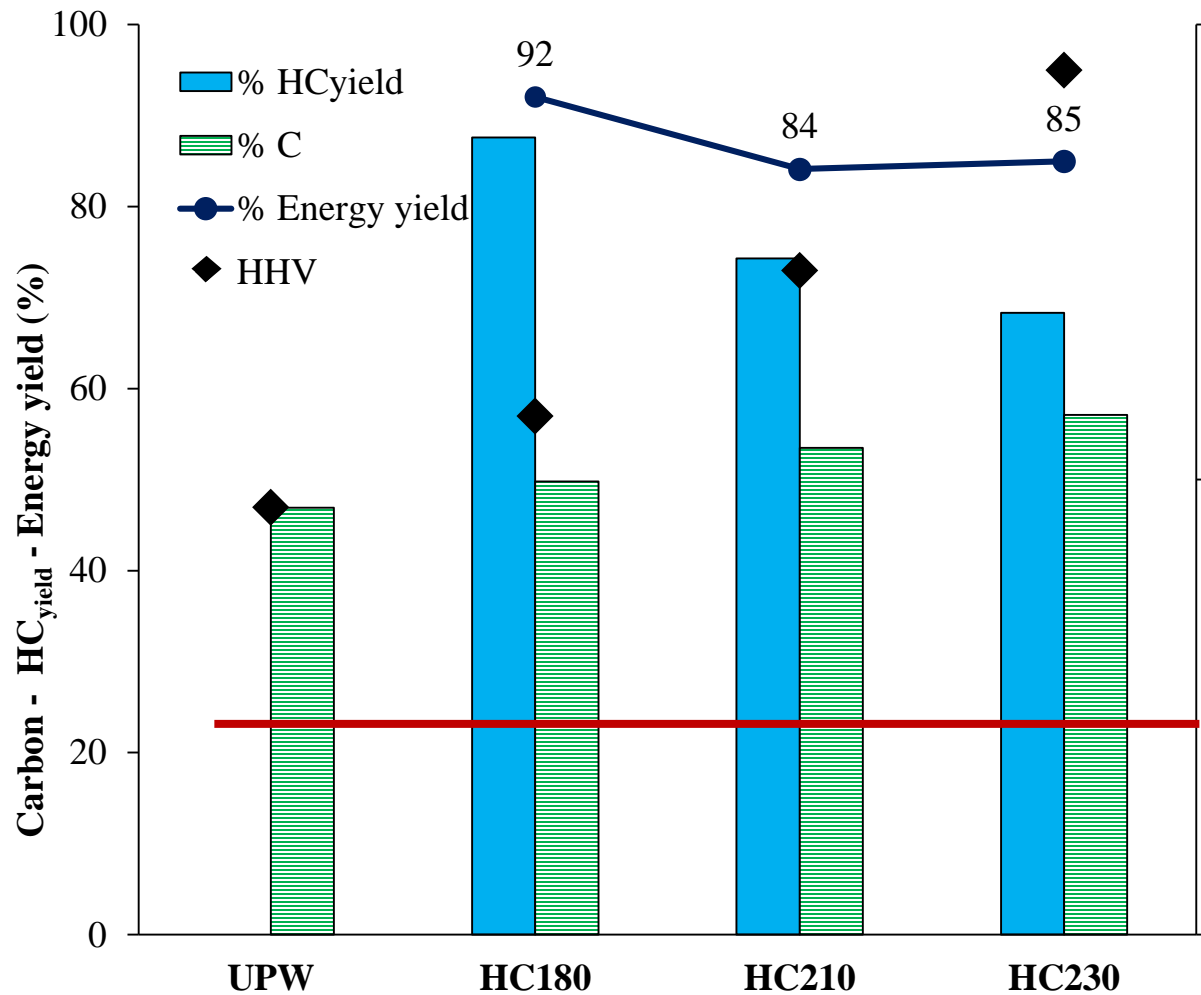
$$HC_{yield} = \frac{M_{HC}}{M_{UPW}} \cdot 100\%$$

$$Carbon (\%) = \frac{\%C_{HC}}{\%C_{UPW}} \cdot 100\%$$

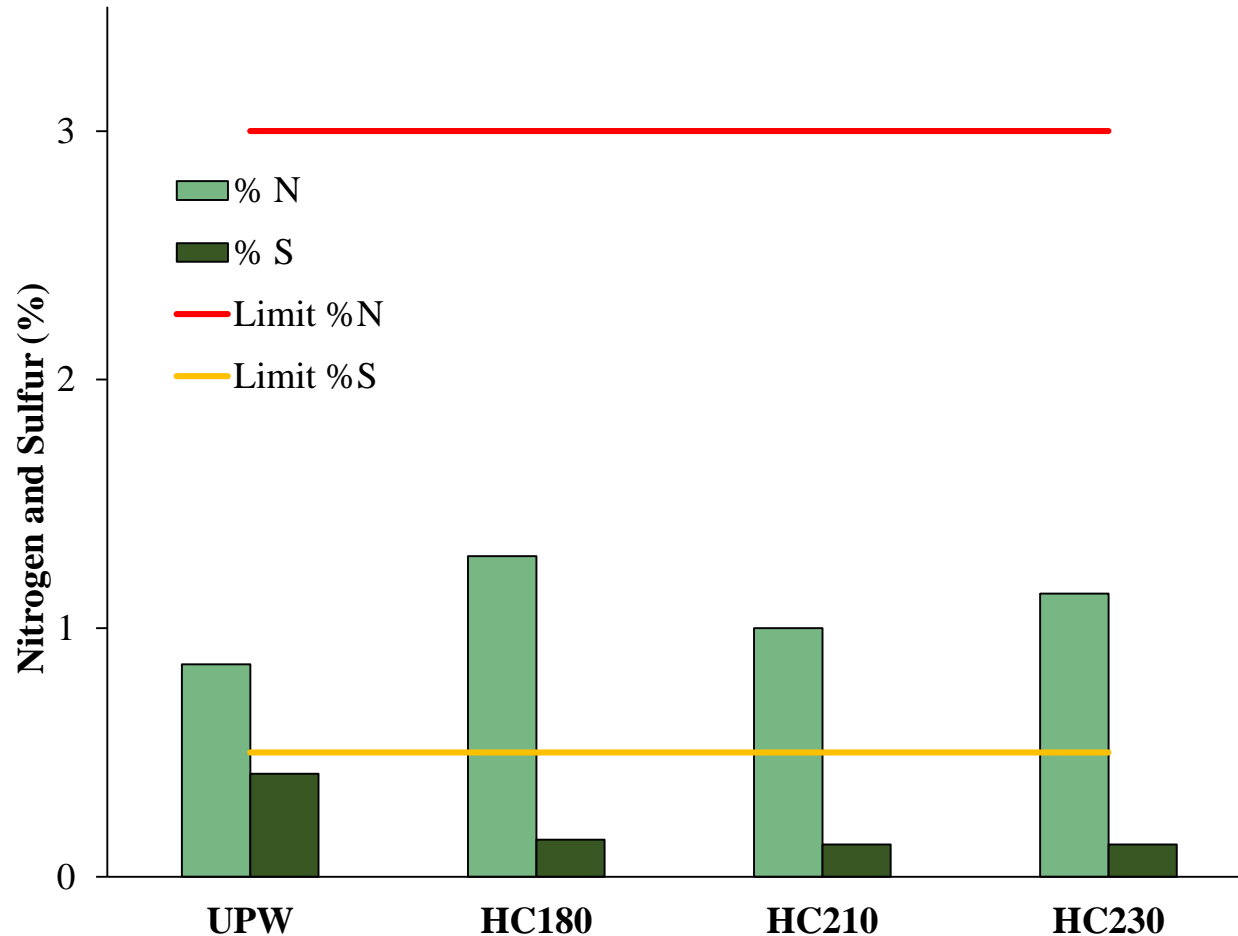
$$HHV (MJ kg^{-1}) = 0,3491 \cdot \%C + 1,1783 \cdot \%H + 0,1005 \cdot \%S - 0,0151 \cdot \%N - 0,0211 \cdot \%Ash$$

$$Energy_{yield} (MJ kg^{-1}) = HHV_{HC} \cdot Y_{HC}$$

Energy and elemental analysis

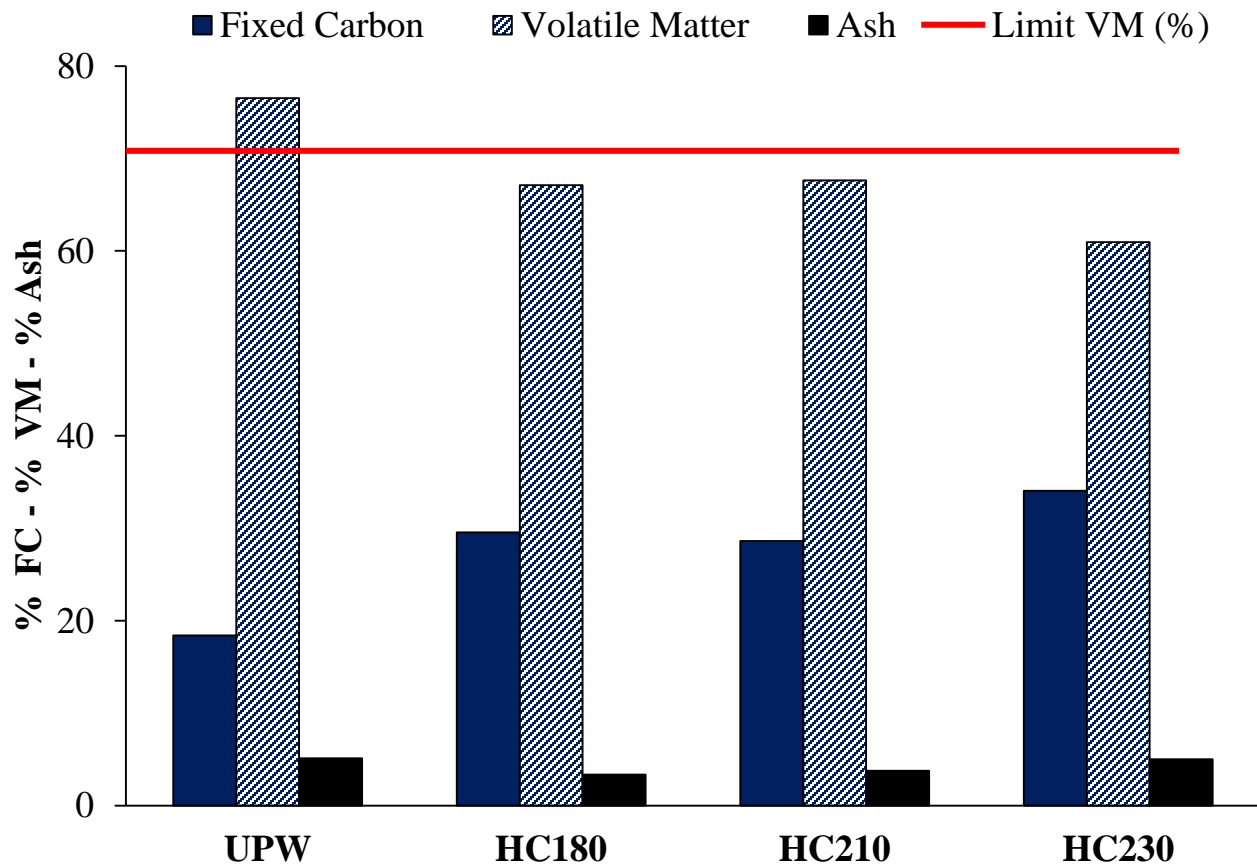


Nitrogen and Sulfur content



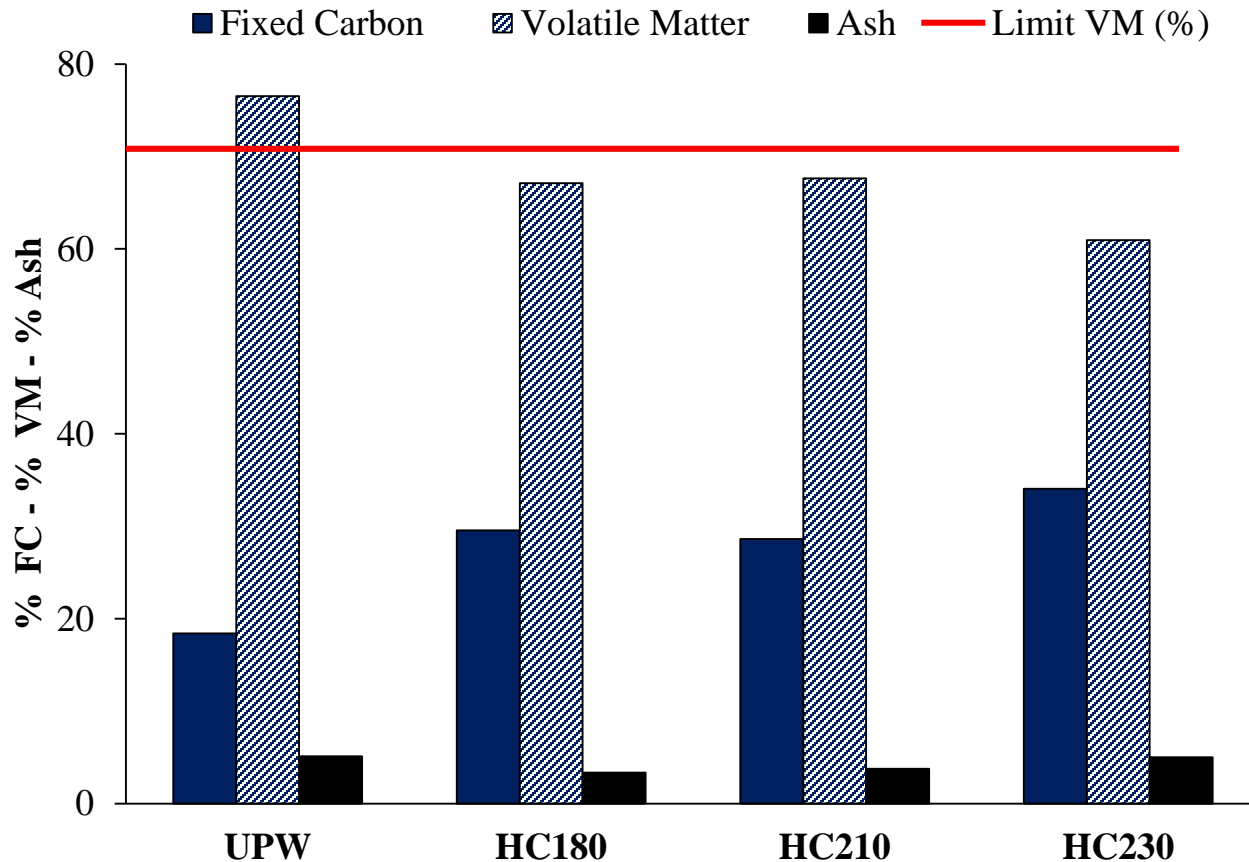
	UPW	HC180	HC210	HC230
HHV > 17 MJ kg ⁻¹	✓	✓	✓	✓
Nitrogen < 3%	✓	✓	✓	✓
Sulfur < 0.5%	✓	✓	✓	✓
Volatile matter < 75%				

Proximal analysis



	UPW	HC180	HC210	HC230
HHV > 17 MJ kg ⁻¹	✓	✓	✓	✓
Nitrogen < 3%	✓	✓	✓	✓
Sulfur < 0.5%	✓	✓	✓	✓
Volatile matter < 75%	✗	✓	✓	✓

Proximal analysis



Ash content



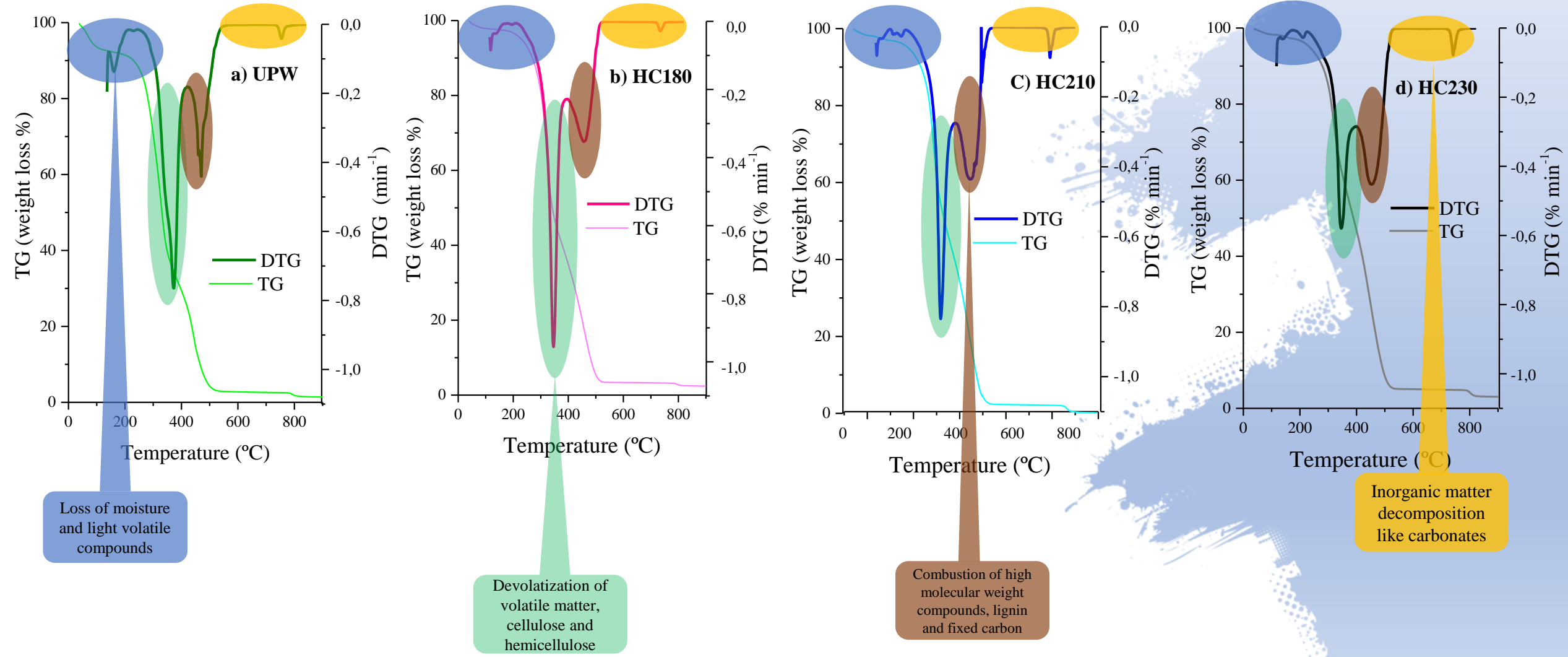
5 – 35%

$$\text{Alkali (kg GJ}^{-1}\text{)} = \frac{1 \cdot 10^6}{\text{HHV (kJ kg}^{-1}\text{)}} \cdot \frac{\% \text{ Ash}}{100} \cdot \left(\frac{\% \text{K}_2\text{O} + \% \text{Na}_2\text{O}}{100} \right)$$

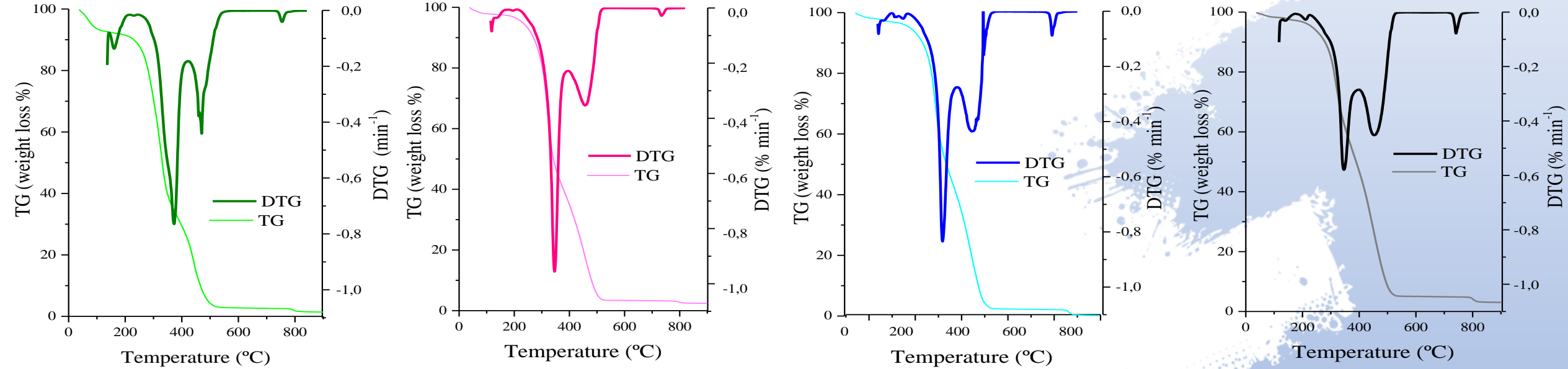
	UPW	HC180	HC210	HC230
Alkali(kg GJ⁻¹)	0.30	0.09	0.07	0.07



Thermogravimetric and differential TG profiles



Thermogravimetric and differential TG profiles



	UPW	HC180	HC210	HC230
T_i (°C)	239	242	251	254
T_m (°C)	326	325	318	313
T_b (°C)	533	528	528	536
$CCI \cdot 10^{-7}$ ($\text{min}^{-2} \text{ } ^\circ\text{C}^{-3}$)	7.8	8.0	8.4	9.6
Z_i (% min^3)	8.6	10.6	11.4	11.6
H_j (% min^4)	0.2	0.3	0.4	0.4

HC stability in the combustion



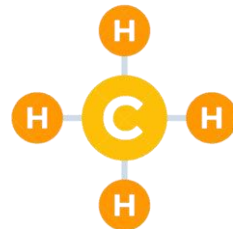
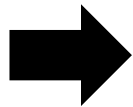
$$CCI (\text{min}^{-2} \cdot \text{ } ^\circ\text{C}^{-3}) = \frac{(dw/dt)_{max} - (dw/dt)_{mean}}{T_i^2 \cdot T_b}$$

$$Z_i = \frac{(dw/dt)_{max}}{t_i \cdot t_{max}}$$

$$H_j = \frac{(dw/dt)_{max}}{t_b \cdot t_{max} \cdot \Delta t_{1/2}}$$

Process water characteristics

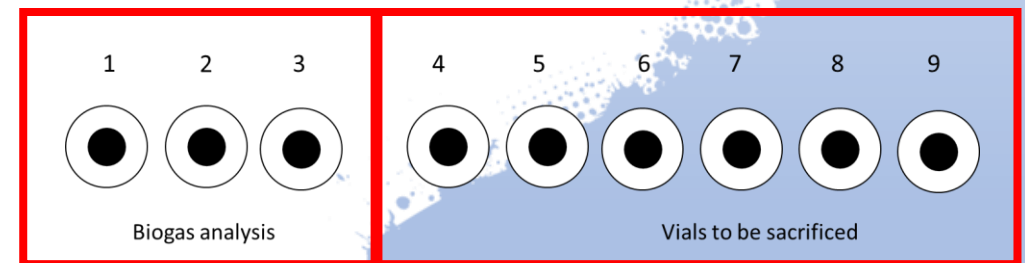
	PW180	PW210	PW230
pH	3.5 ± 0.1	3.4 ± 0.1	3.5 ± 0.1
COD (g L⁻¹)	51.1 ± 1.3	39.3 ± 0.5	44.9 ± 2.4
TOC (g L⁻¹)	21.1 ± 0.1	17.0 ± 0.1	18.4 ± 0.1
TAGV (g L⁻¹)	1.5 ± 0.0	0.9 ± 0.0	0.2 ± 0.0
TS (g L⁻¹)	30.7 ± 0.3	19.3 ± 0.3	21.6 ± 0.4
VS (g L⁻¹)	27.0 ± 0.4	16.1 ± 0.2	18.5 ± 0.3



Biomethane potential test

ISR = 2

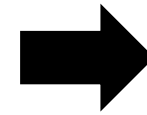
- 15 g VS L⁻¹ granular anaerobic sludge
- 7.5 g VS L⁻¹ substrate



Positive controls

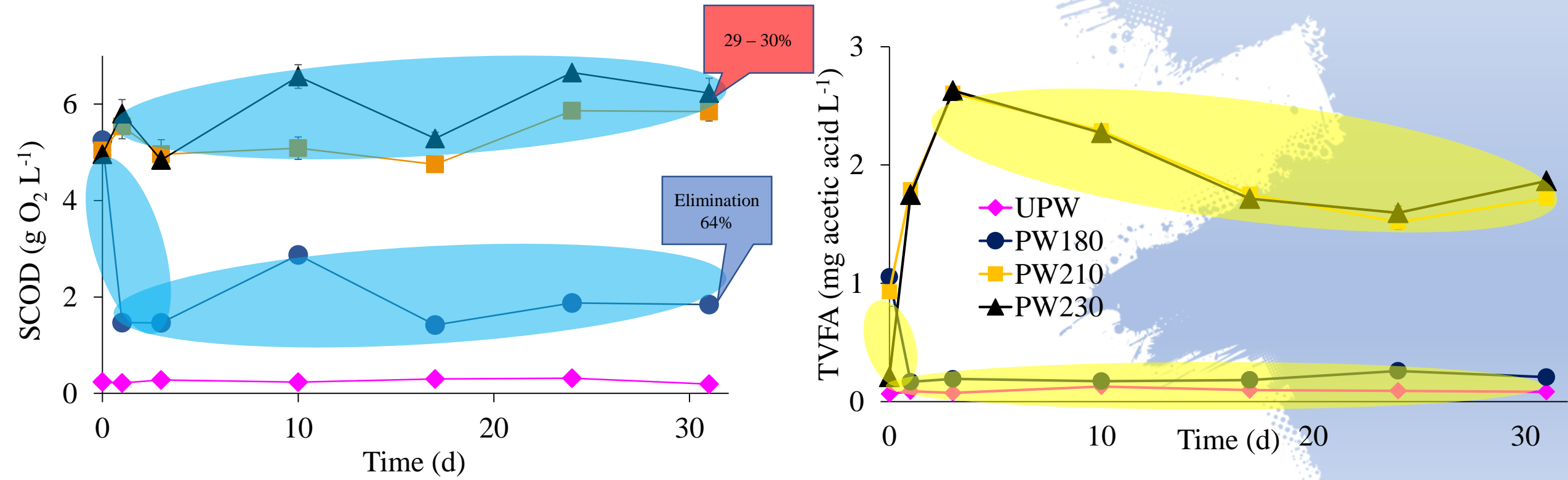
Blanks

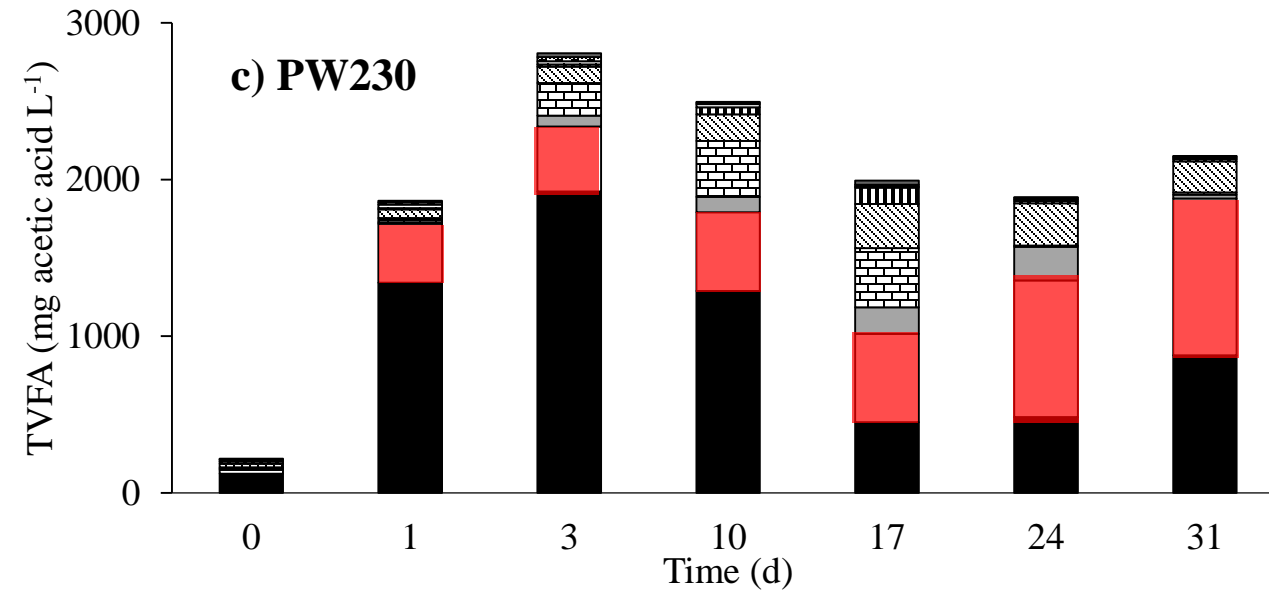
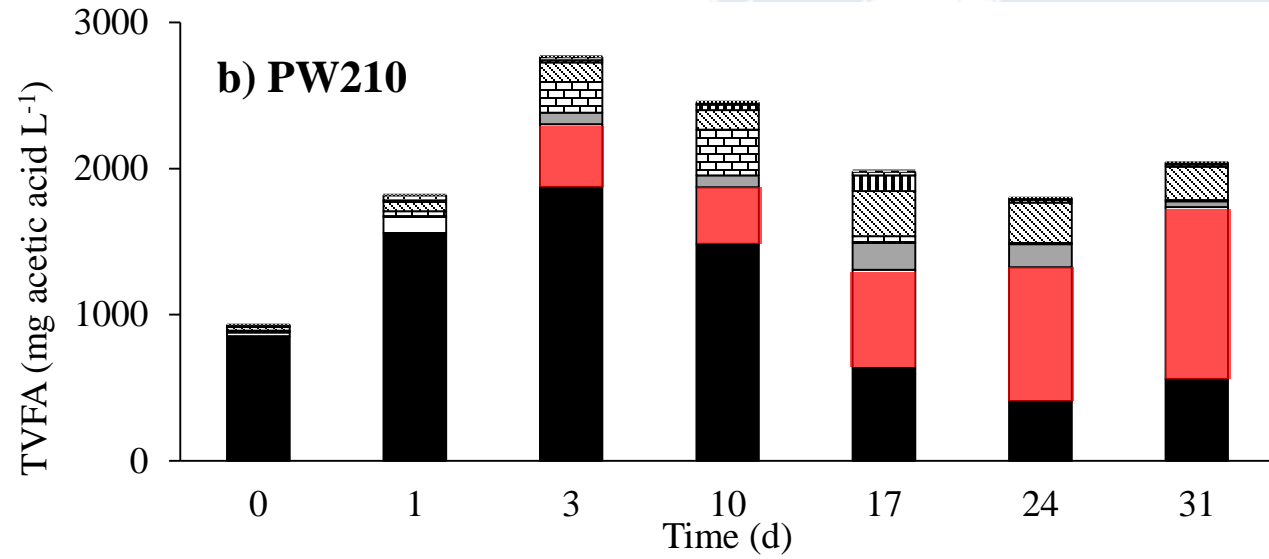
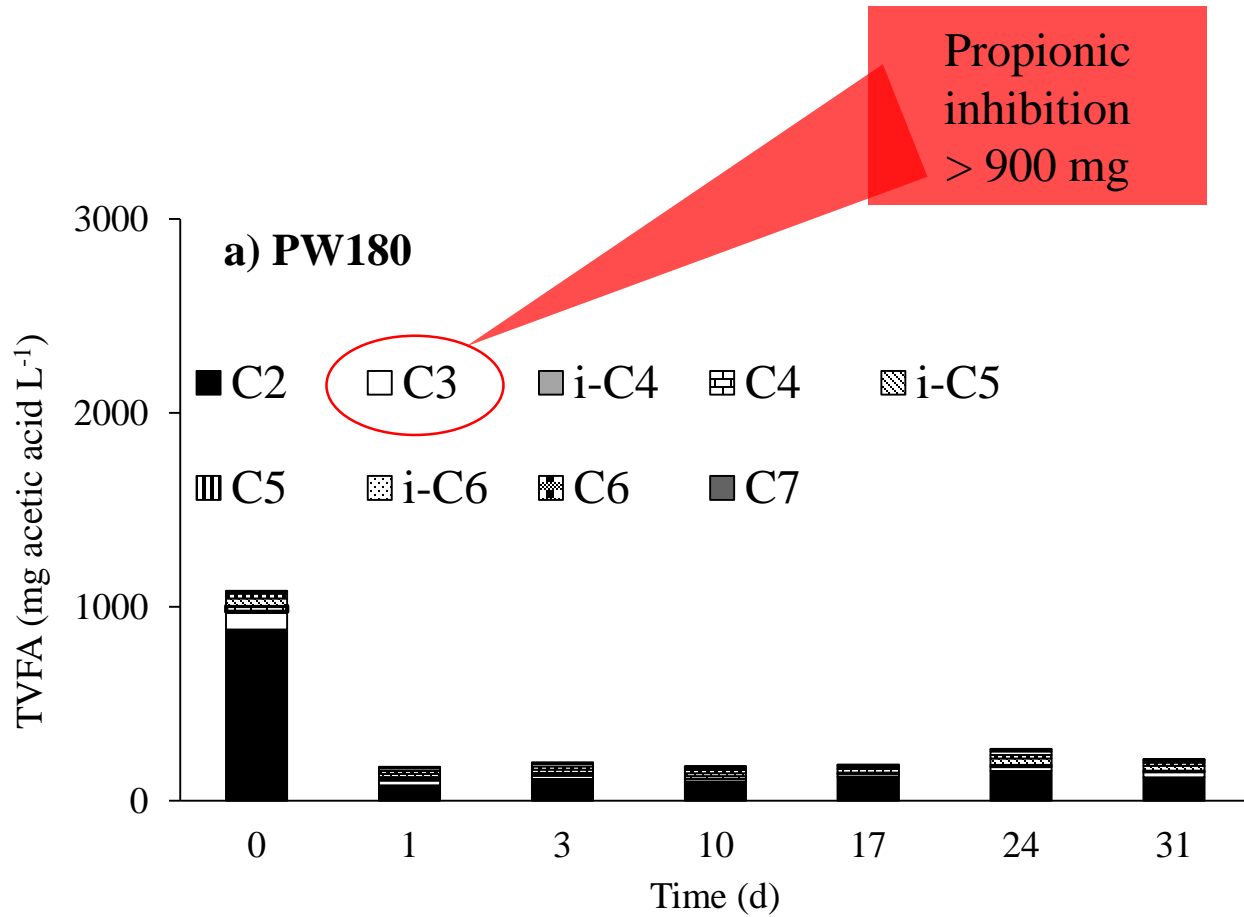
- ✓ pH (7.5 – 7.8)
- ✓ Alkalinity ($> 2.5 \text{ g CaCO}_3 \text{ L}^{-1}$)
- ✓ Total ammonia nitrogen ($1700 \text{ mg L}^{-1} < \text{inhibition values}$)



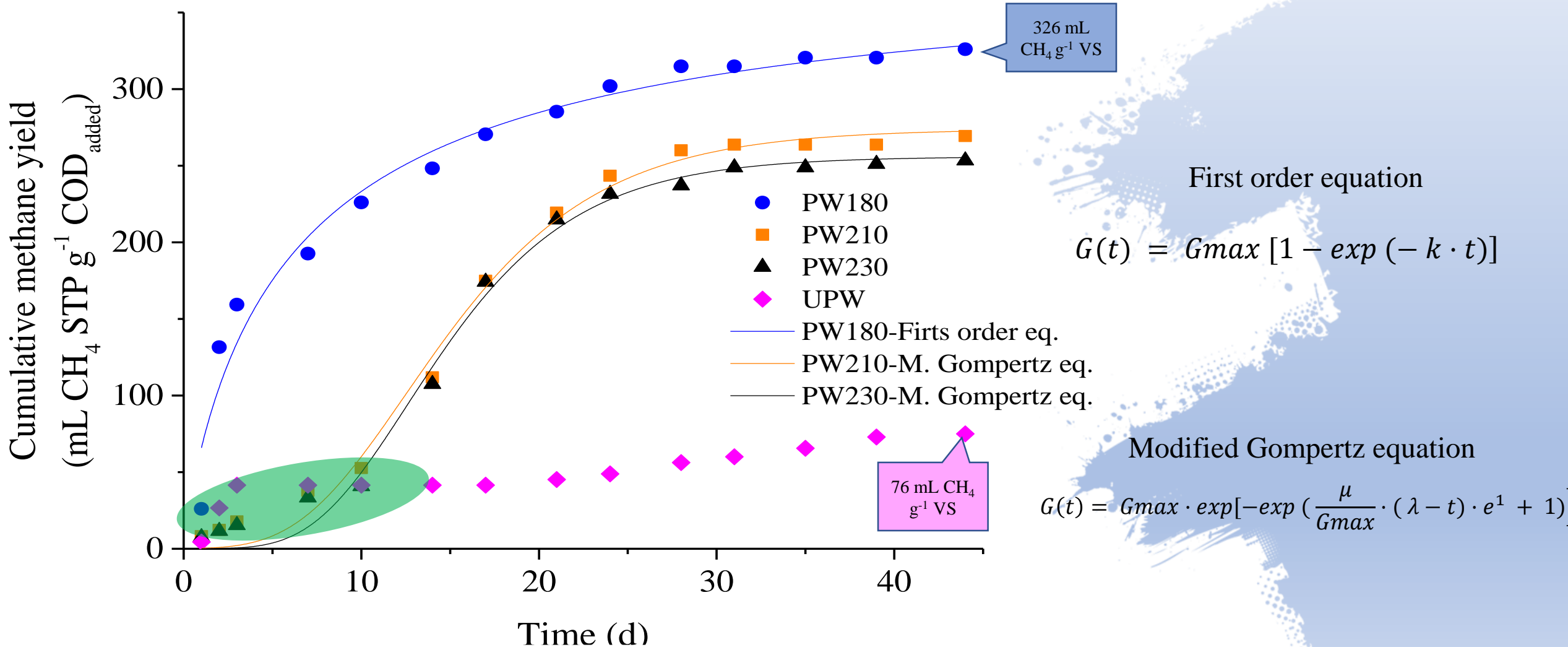
Adequate for the AD process

Time-course of total soluble chemical oxygen demand (COD) and volatile fatty acids (VFA)

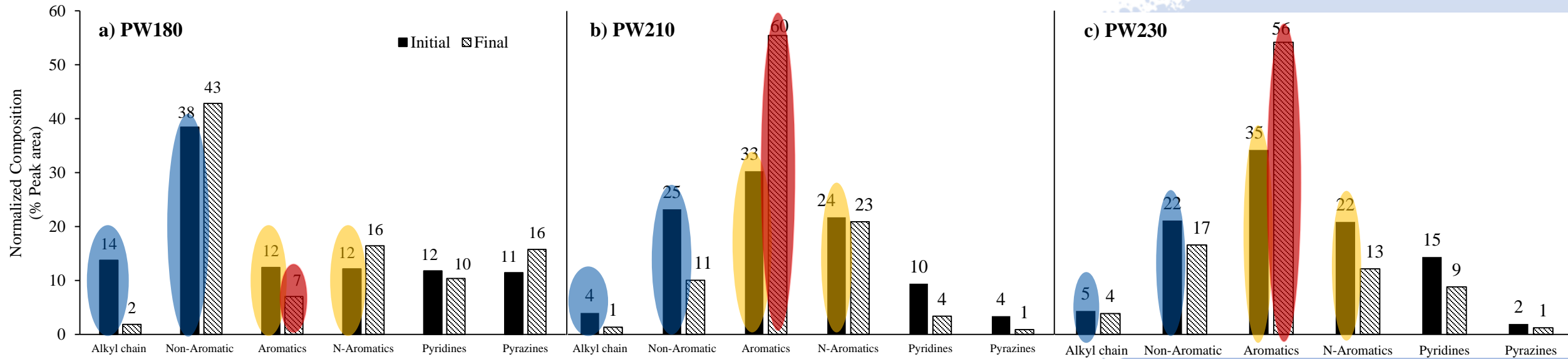




Cumulative methane yield



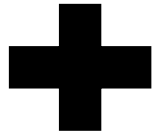
Recalcitrant compounds



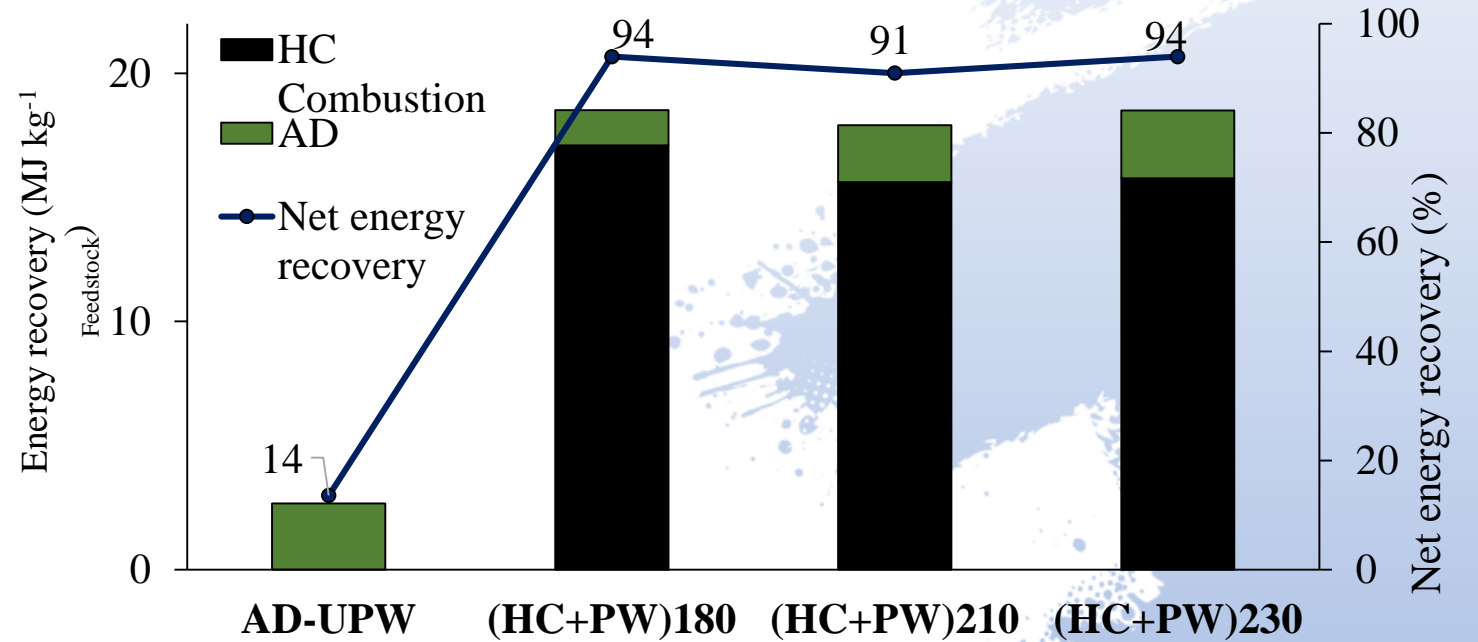
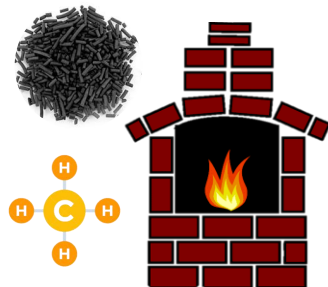
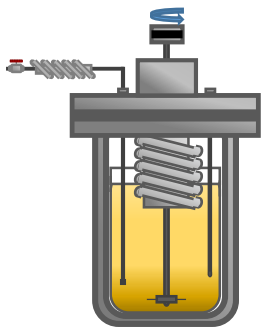
Energy recovery



HC



CH₄



	Energy Input (MJ t ⁻¹ _{feedstock})	Energy Output (MJ t ⁻¹ _{feedstock})		
	HTC reactor	Energy HC	Energy CH ₄	Total output
HTC180	1311	3627	1414	5041
HTC210	1819	3315	2295	5610
HTC230	1662	3348	2734	6082

Conclusions

- ✓ The HC presents better physicochemical properties than the raw material like higher carbon content (50 – 57%), HHV values (21 – 25 MJ kg⁻¹) and low ash (< 5%), nitrogen (< 1.3%) and sulfur (< 0.2%).
- ✓ The HCs show high stability that together with low ash content prevent fouling and slagging in the boilers.
- ✓ The AD of the PW at low temperatures have higher organic matter elimination yields (up to 65%), while the higher temperatures affect negatively the removal of organic compound due the high recalcitrant organic compounds content.
- ✓ The energy balance shows the possibility of integrating these two processes with high energy recovery yields (91 – 94%).
- ✓ The energy obtain for the combustion of HCs and methane is 3 times greater than the energy required to carry out the entire proposed process
- ✓ Coupling thermochemical and biological processes (HTC + AD) could open new avenues to produce renewable energy with higher energy recovery's and higher organic matter removal and promote the development of a circular economy with zero waste.



Urban Bioeconomy: from Biowaste to Biofuels and Bioproducts of Industrial Interest

Acknowledgements

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Thank you



**Urban bioeconomy:
transformation of biowaste
into biofuels and bioproducts
of industrial interest**



**“The earth is a fine
place and worth
fighting for”**

Ernest
Hemingway