

Hydrogen production from bio-oil aqueous phase steam reforming over agglomerated Co-Cr/SBA-15 catalysts

Workshop BIO3, Objective 4

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18 de Diciembre 2020



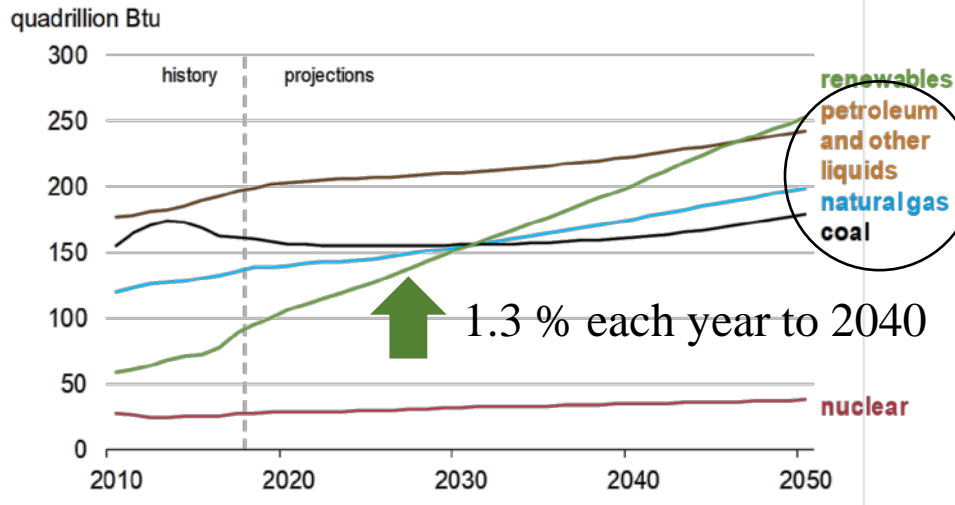
Introduction

Experimental

Results

Conclusions

Current energy situation



fossil fuels



Emission of greenhouse gases



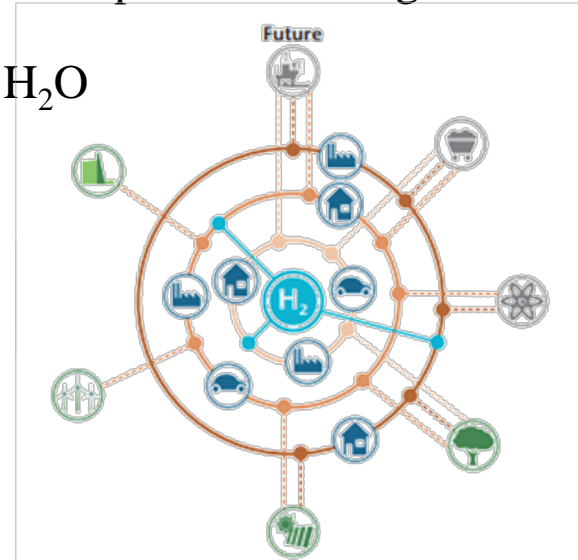
Alternatives?





- Most abundant gas in universe → Not available in free form
- Fuel with the maximum energy content per unit of weight
- Clean fuel → $\text{H}_2 + \frac{1}{2} \text{O}_2 \rightarrow \text{H}_2\text{O}$

Hydrogen production from renewable sources can lead to a sustainable energy system in the near future



Currently, there are different technologies for hydrogen production from this feedstocks:

- Fossil fuels
- Water
- Biomass/waste

Thermochemical processes

Pyrolysis

HTL

Gasification

Main
product

Gas

Liquid

Solid

Bio-oil

Revalorization by
catalytic reforming



- Larger energy density than biomass
- Low heating power
- Corrosivity
- Instability

Low-quality fuel

• Aqueous fraction

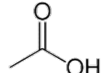
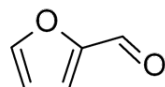
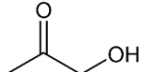
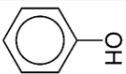


• Organic fraction



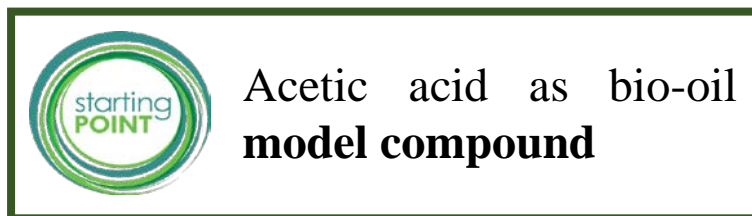


Different and complex compositions

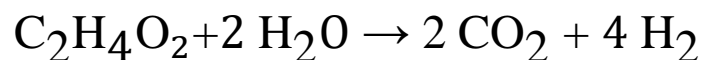
Aqueous phase composition	Typical compound	Typical concentration (wt. %)
Carboxylic acids		19.1-22.9
Aldehydes		0.5-5.5
Furans		
Ketones		13.9-17.5
Phenols		2.0-13.4

Alvarez J., et al. Fuel 128 (2014) 162-9

Remón J., et al. Int. J. of Hydrogen Ener., 40 (2015) 5593-608



Catalytic steam reforming of acetic acid as model compound



Secondary reactions

- Methanation $3\text{H}_2 + \text{CO} \rightarrow \text{CH}_4 + \text{H}_2\text{O}$
- Coke formation $2\text{CO} \leftrightarrow \text{CO}_2 + \text{C}$
- Water-gas shift $\text{CO} + \text{H}_2\text{O} \leftrightarrow \text{CO}_2 + \text{H}_2$

Design of suitable catalysts

CHALLENGE

Reforming catalysts

- Responsibility for cracking not only C-C and C-H bonds but also O-H bonds
- High activity
- High selectivity towards H₂
- Low deactivation (high resistance to coking and sintering)

Active phase

44 Ru Ruthenium 101.07	45 Rh Rhodium 102.906
46 Pd Palladium 106.42	79 Pt Platinum 195.084

Noble metals

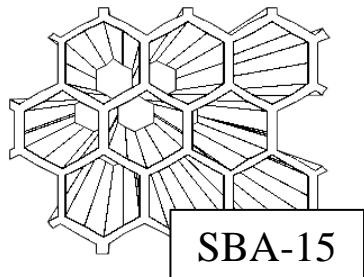
High **activity**
but high **cost**

27 Co Cobalt 58.933	28 Ni Nickel 58.693
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Transition metals

Reasonable **activity** and
lower **cost** than noble metal

Support



- Good results in oxygenated hydrocarbons steam reforming
Vizcaíno, A.J., et al. *Catalysis Today* 146(1-2) (2009) 63-70
- Improve metal dispersion and decrease sintering
Yang, X., et al. *Catalysts* 5 (2015) 1721–1736

Inconvenience?

These reforming catalysts are usually prepared as **fine powders** being **not appropriate** for use **at industrial scale**



High pressure drop



Solution

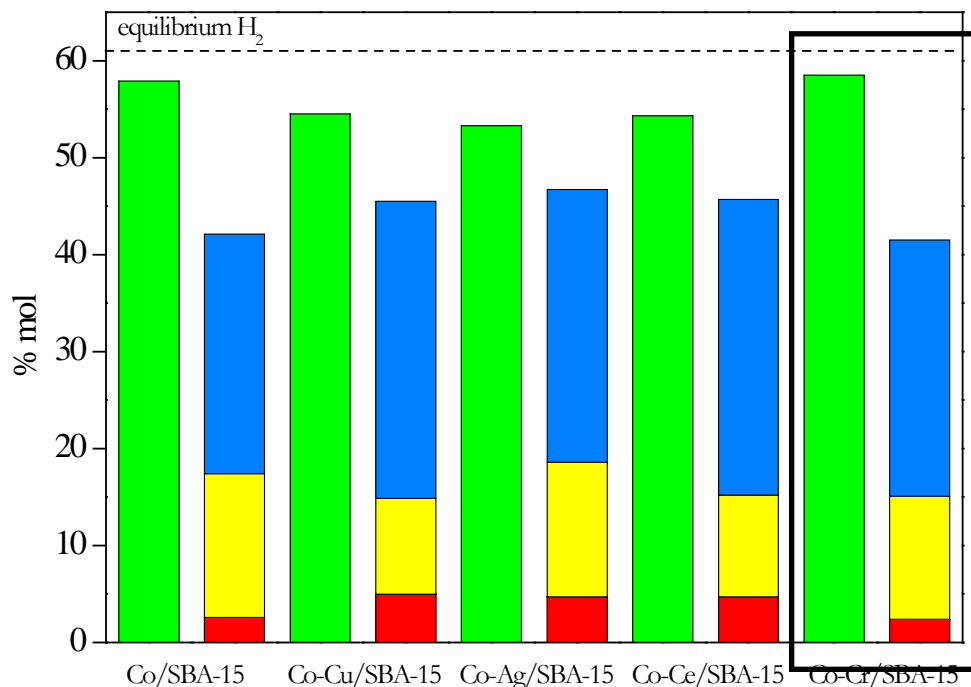
Catalysts
agglomeration
using binders



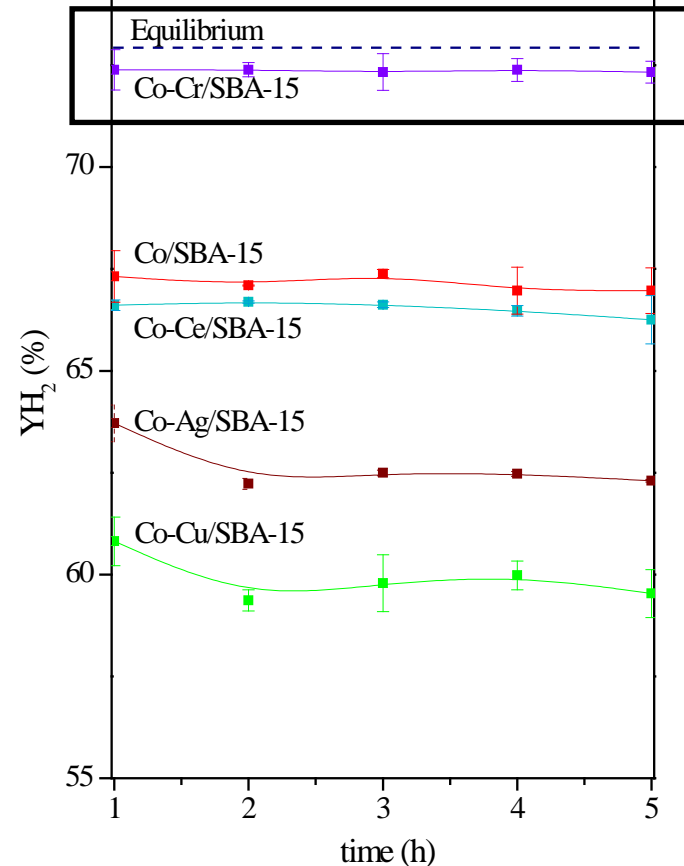
Cr addition enhances the catalytic performance towards hydrogen

Previous works

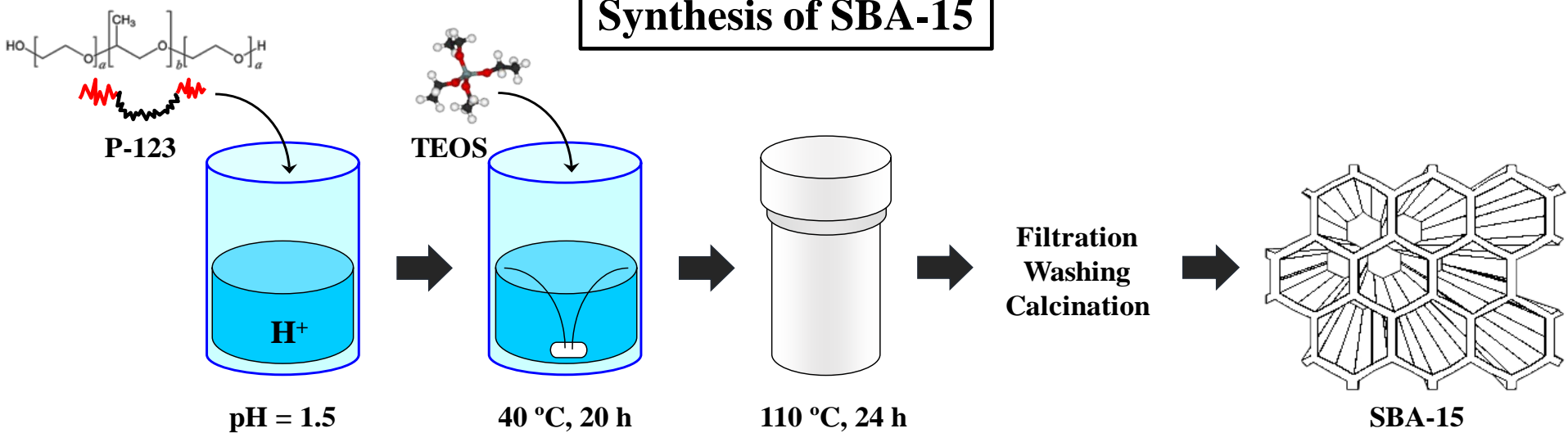
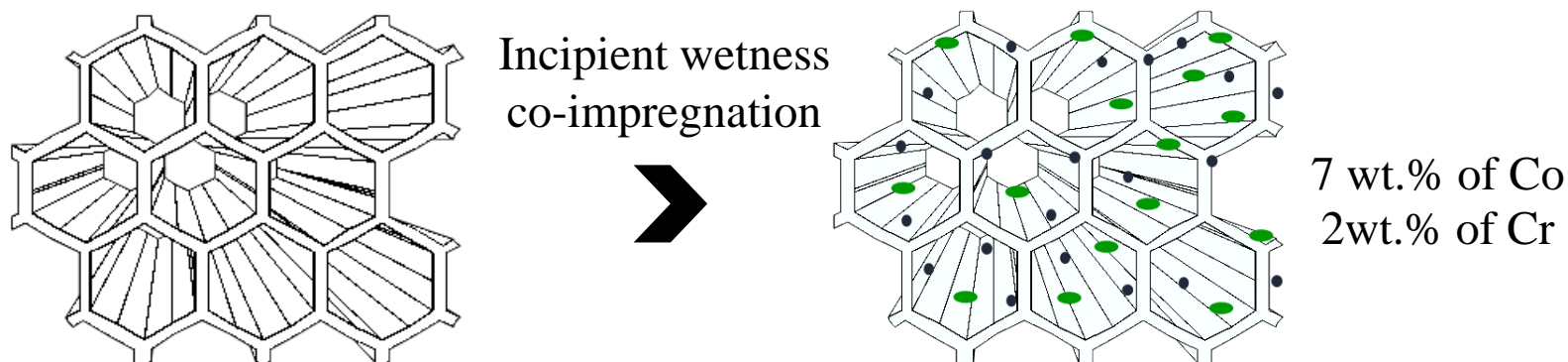
■ H₂
■ CO₂
■ CO
 ■ CH₄



Megía P.J., Carrero A., Calles J.A., Vizcaíno A.J.
Catalysts, 9 (12), 1013;



Preparation of **agglomerated Co-Cr/SBA-15** using bentonite and methylcellulose as binder through acetic acid steam reforming

Synthesis of SBA-15**Catalysts preparation**

Catalysts agglomeration procedure

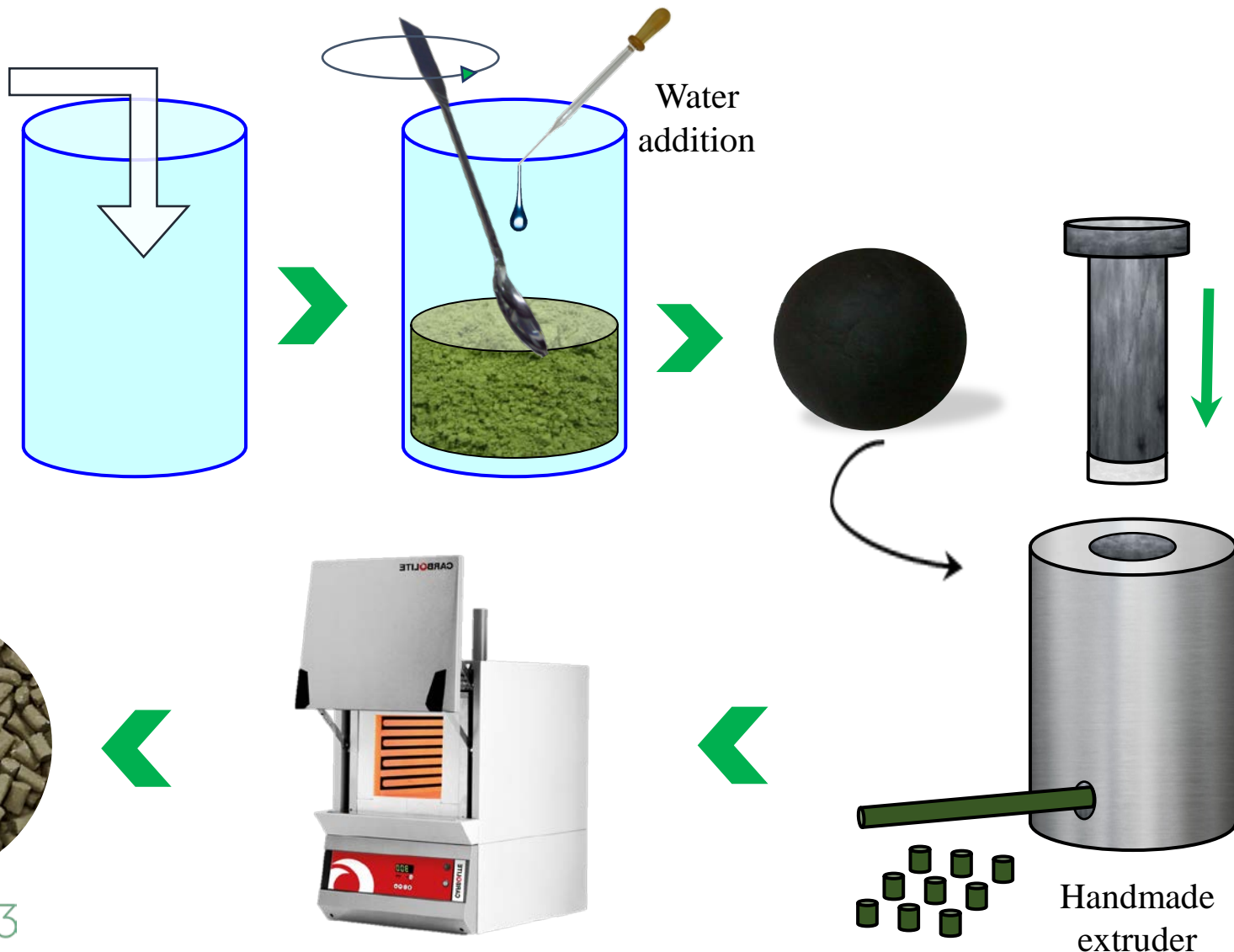
Co-Cr/SBA-15



Methylcellulose



Bentonite



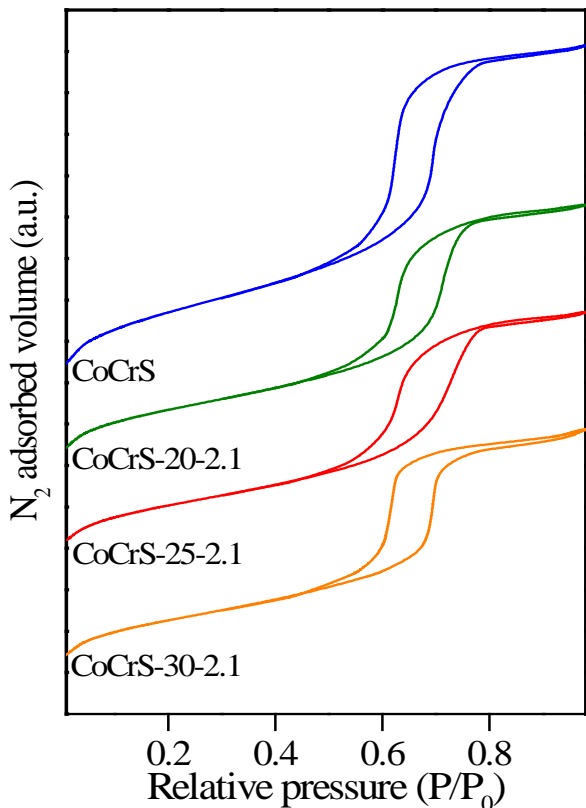
Catalytic tests**Feed system****Analysis system**

Online Micro-GC: gas outlet stream
GC Varian CP-3380: liquid stream

Fixed-bed reactor

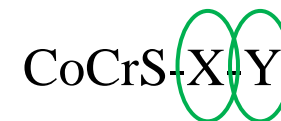
$T=600^{\circ}\text{C}$, atmospheric pressure, 5h (TOS). Prior to reaction: reduction under H_2



Catalysts characterization

Type IV isotherm
H1-type hysteresis loop

Preservation of the initial
mesoporous structure



X = wt. % of bentonite

Y = effective diameter (mm)

Physicochemical properties

Sample	Co (wt.%) ^a	Cr (wt.%) ^a	S _{BET} (m ² /g)	V _p ^b (cm ³ /g)	D _p ^c (nm)	D _{Co₃O₄} ^c (nm)
CoCrS	6.4	1.7	490	0.7	5.5	7.1
CoCrS-20-2.1	5.3	1.4				8.1
CoCrS-25-2.1	4.9	1.3				8.0
CoCrS-30-2.1	4.5	1.2	322	0.5	5.5	8.1

^a Determined by ICP-AES in calcined samples

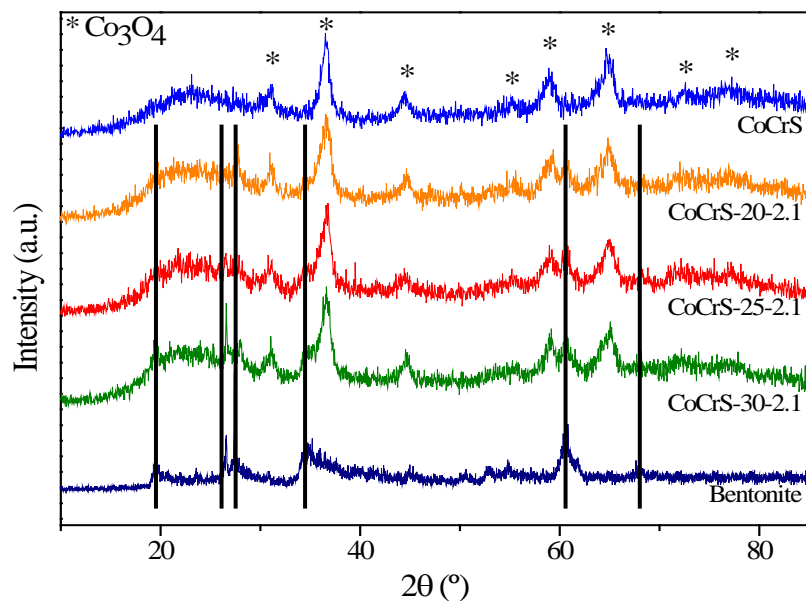
^b Pore Volume measured at P/P₀ = 0.97

^c BJH desorption average pore diameter

^d Determined from XRD of calcined catalysts by Scherrer equation from the (

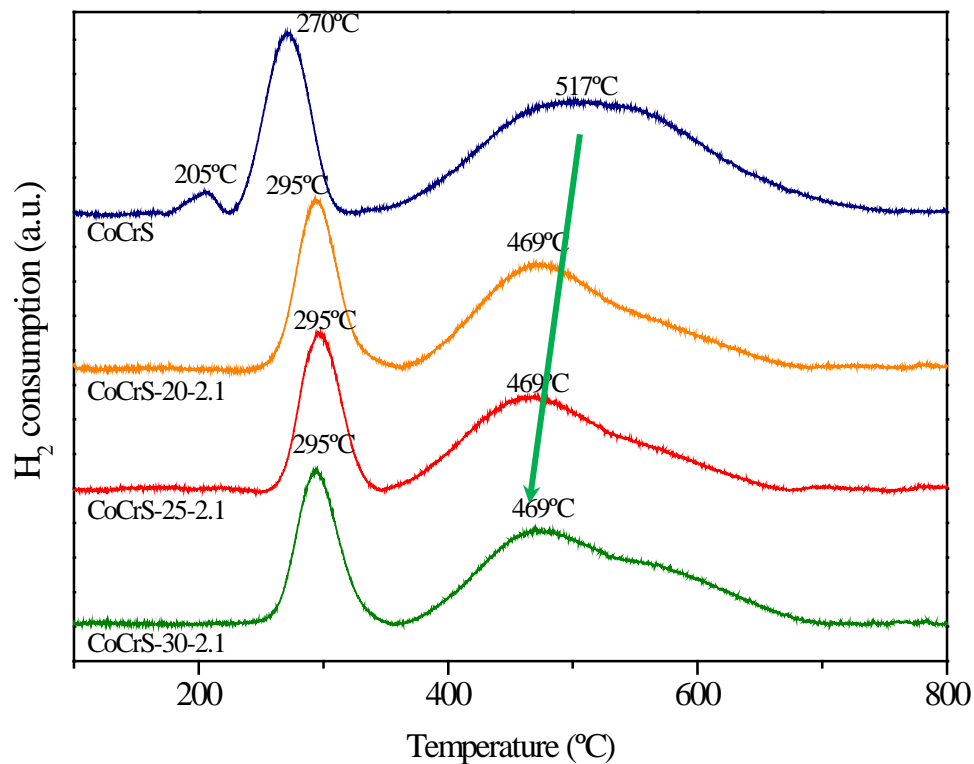
Higher calcination
temperatures (>100 °C)

Similar to
powder sample O₄

Catalysts characterization

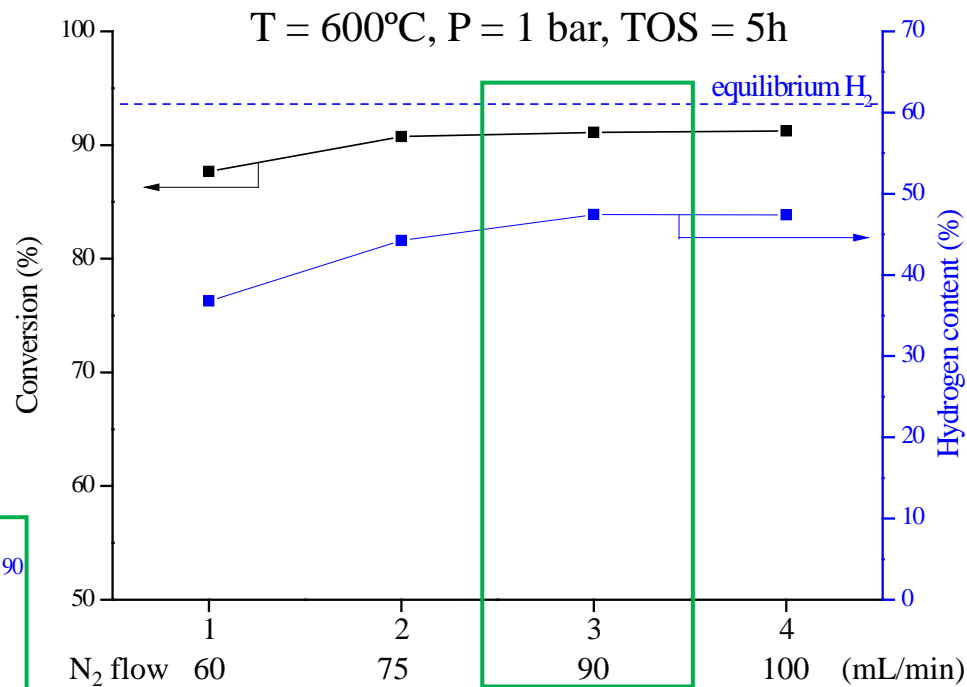
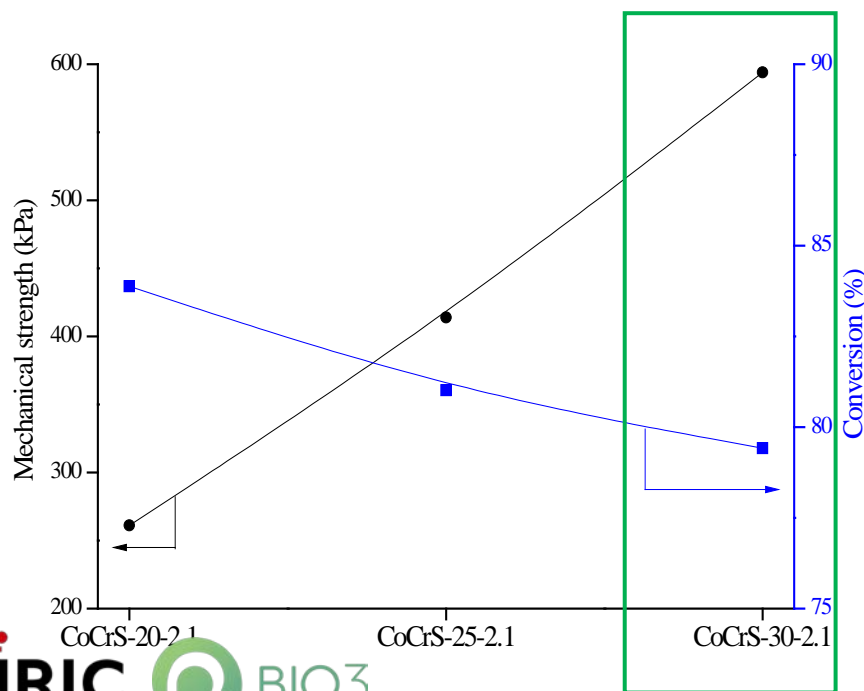
Decrease in the reduction
temperature in extruded catalysts

Montmorillonite (Bentonite)



External diffusion effectsConstant WHSV = 32.1 h⁻¹

Conditions	m _{catalyst} (g)	Q _{feed} (mL/min)	N ₂ flow (mL/min)
1	0.300	0.0750	60
2	0.375	0.0935	75
3	0.450	0.1125	90
4	0.500	0.1250	100

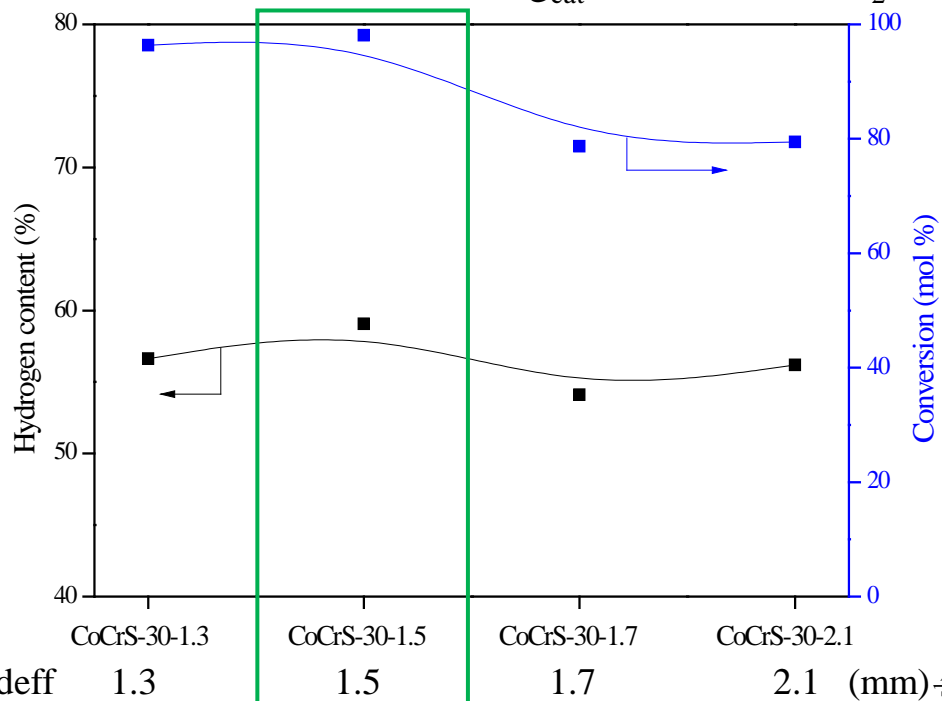


CoCrS-20-2.1

CoCrS-30-2.1 highest mechanical strength
 Lowest fine formation after 5h TOS
 Lower conversion than the other samples

Internal diffusion effects

$T = 600^{\circ}\text{C}$, TOS = 5h, $0.45 \text{ g}_{\text{cat}}$ & 90 mL/min N_2



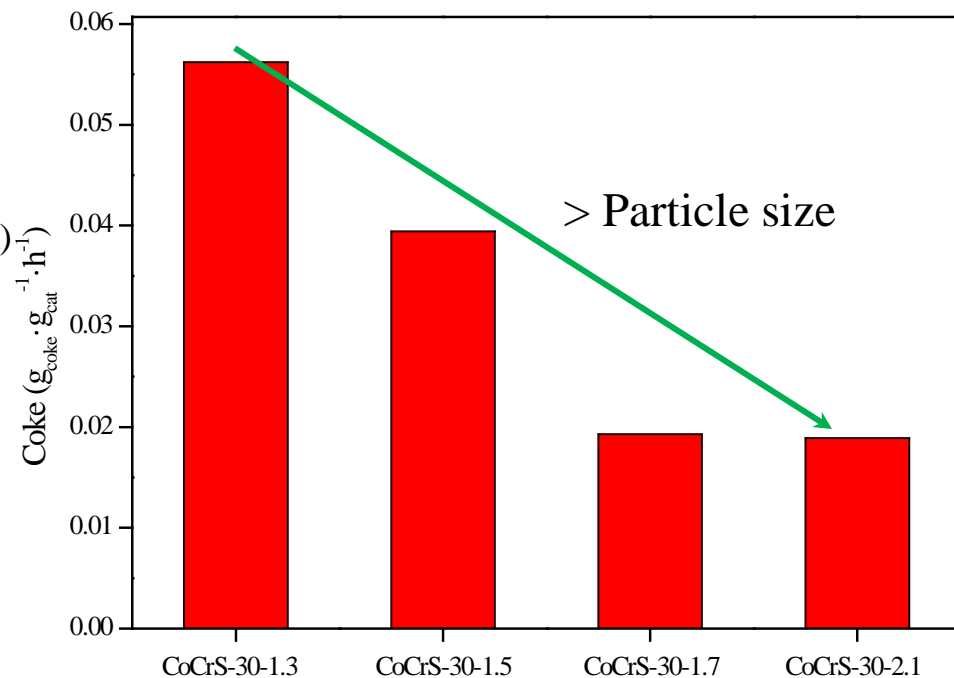
↓ Particle size → ↑ Coke formation

- Higher conversion
- Non-uniform coke distribution (preferably in external surface)

Different effective diameters
1.3-2.1 mm

Similar hydrogen content

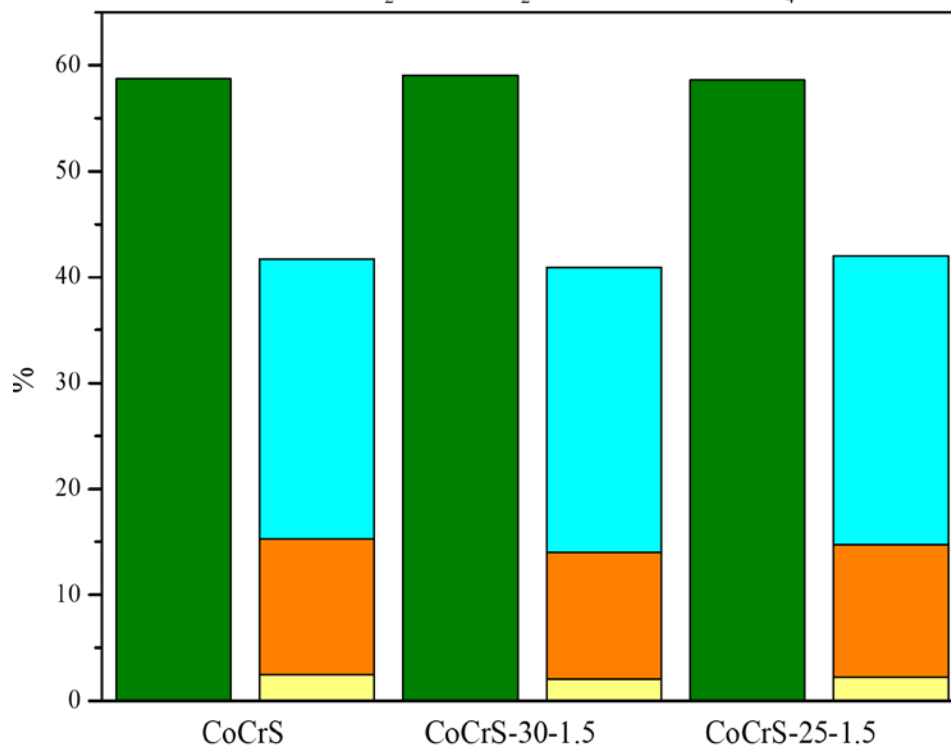
↓ Particle size → ↑ Conversion



Forzatti P., Lietti L. Catal. Today 52 (1999) 165-81.

Comparison with the powder sample

T = 600°C, P = 1 bar, TOS = 5h

■ H₂ ■ CO₂ ■ CO ■ CH₄

Similar conversion & gas product distribution

Conversion (5h)

CoCrS

CoCrS-30-1.5

CoCrS-25-1.5

(mol %)

Successful agglomeration process → **CoCrS-30-1.5** (higher mechanical strength)

D_{eff}
0.15 cm

0.45 g_{cat}
0.1125 mL/min



30 wt.% of
bentonite

Similar results
to powdered
sample

↪ **30 wt.% bentonite** hardly decreased the acetic acid conversion compared to 20 wt.% while the **mechanical strength** almost was **tripled**.

↪ **CoCrS-30-1.5** showed a good performance for hydrogen production and similar conversion compared to powder sample

Suitable
agglomeration
process

